

# EGR-GAS FLOW RATE ESTIMATION APPARATUS FOR INTERNAL COMBUSTION ENGINE

## BACKGROUND OF THE INVENTION

### Field of the Invention

The present invention relates to an EGR-gas flow rate estimation apparatus, for an internal combustion engine, which estimates the flow-rate of EGR gas flowing from an exhaust circulation pipe to an intake passage of the internal combustion engine.

### Description of the Related Art

Conventionally, there has been widely known an EGR apparatus which circulates a portion of exhaust gas of an internal combustion engine to an intake passage via an exhaust circulation pipe, in order to reduce the amount of nitrogen oxides ( $\text{NO}_x$ ) discharged from the engine. Such an EGR apparatus is applied to both spark-ignition engines and diesel engines. In this case, the flow rate of EGR gas is controlled by changing the opening (effective opening area) of an EGR control valve interposed in the exhaust circulation pipe.

Such an EGR apparatus is designed to estimate the flow rate of EGR gas flowing into the intake passage and measure the flow rate of new air flowing into the intake passage; obtain an EGR ratio, which is the ratio of the EGR gas flow rate to the flow rate of all gases taken in by an engine (i.e., a mixture of new air and EGR gas, and hereinafter, also referred to as "intake air"), on the basis of the estimated EGR gas flow rate and the measured new air flow rate; and control the EGR gas flow rate on the basis of the EGR ratio. Accordingly, accuracy of the estimation of the flow rate

of EGR gas flowing into the intake passage is extremely important for engine controls such as control of the EGR gas flow rate. In view of the above, a conventional apparatus is designed to estimate the EGR gas flow rate on the basis of a differential pressure across the EGR control valve (hereinafter referred to as "across differential pressure") and the opening of the EGR control valve (see, for example, Japanese Patent Application Laid-Open (*kokai*) No. 2001-280202 (paragraph 0005 and page 4)). The conventional apparatus is designed to estimate the EGR gas flow rate, by using, as the across differential pressure, the difference between a pressure detected by means of a boost sensor (intake pressure sensor) disposed in the intake passage and a pressure detected by means of a pressure sensor disposed at an appropriate position upstream of the EGR control valve. However, in some cases, the differential pressure between points immediately before and after the EGR control valve may greatly differ from the across differential pressure used for estimation of the EGR gas flow rate, stemming from pipe friction produced between the EGR gas and the exhaust circulation pipe. In such a case, the EGR gas flow rate cannot be accurately estimated.

In particular, an error involved in estimation of the EGR gas flow rate caused by the pipe friction increases, and thus, estimation accuracy of the EGR gas flow rate deteriorates, in the case where the flow rate of EGR gas passing through the EGR control valve (accordingly, the flow rate of EGR gas flowing into the intake passage) is estimated by use of a general formula relating the flow rate of a compressible fluid passing through a throttle portion (EGR control valve), in which the flow rate of the compressible fluid is represented on the basis of an upstream pressure of

the compressible fluid at a point immediately before the throttle portion and a downstream pressure of the compressible fluid at a point immediately after the throttle portion.

## SUMMARY OF THE INVENTION

In view of the foregoing, an object of the present invention is to provide an EGR-gas flow rate estimation apparatus, for an internal combustion engine, which can accurately estimate the flow rate of EGR gas flowing into the intake passage of the engine via an EGR control valve, by considering the above-described pipe friction.

The present invention provides an EGR-gas flow rate estimation apparatus for an internal combustion engine which has an exhaust circulation pipe connected between an exhaust passage and an intake passage, and an EGR control valve interposed in the exhaust circulation pipe and having a throttle portion for controlling flow rate of EGR gas flowing through the exhaust circulation pipe. The EGR-gas flow rate estimation apparatus comprises: upstream-gas-pressure obtaining means for obtaining, as an upstream-side gas pressure, a pressure of EGR gas on the upstream side of the EGR control valve; downstream-gas-pressure obtaining means for obtaining, as a downstream-side gas pressure, a pressure of EGR gas on the downstream side of the EGR control valve; provisional-EGR-gas-flow-rate estimation means for estimating, as a provisional EGR gas flow rate, a flow rate of EGR gas passing through the EGR control valve, by use of a general formula which represents a flow rate of a compressible fluid passing through a throttle portion on the basis of an upstream pressure of the compressible fluid at a point immediately before

the throttle portion and a downstream pressure of the compressible fluid at a point immediately after the throttle portion, the provisional-EGR-gas-flow-rate estimation means employing the obtained upstream-side gas pressure as the upstream pressure of the compressible fluid in the general formula, and the obtained downstream-side gas pressure as the downstream pressure of the compressible fluid in the general formula; and EGR-gas flow rate estimation means for estimating the flow rate of EGR gas flowing from the exhaust circulation pipe into the intake passage, by correcting an error which is contained in the estimated provisional EGR gas flow rate and which is caused by pipe friction between the exhaust circulation pipe and the EGR gas.

According to the general formula which represents the flow rate of a compressible fluid passing through a throttle portion, the flow rate of the compressible fluid passing through the throttle portion can be accurately obtained on the basis of an upstream pressure of the compressible fluid at a point immediately before the throttle portion and a downstream pressure of the compressible fluid at a point immediately after the throttle portion.

Therefore, the present apparatus obtains a gas pressure (e.g., exhaust pressure) at a certain location (e.g., exhaust passage) on the upstream side of the throttle portion of the EGR control valve, and employs the obtained gas pressure as the upstream pressure of the compressible fluid at a point immediately before the throttle portion. Further, the present apparatus obtains a gas pressure at a certain location (e.g., intake passage) on the downstream side of the throttle portion of the EGR control valve, and employs the obtained gas pressure as the downstream pressure of the compressible fluid at a point immediately after the throttle portion, whereby

the present apparatus obtains a tentative EGR gas flow rate.

Subsequently, the present apparatus corrects an error which is contained in the estimated provisional EGR gas flow rate and which is caused by the pipe friction between the exhaust circulation pipe and the EGR gas, to thereby estimate the flow rate of the EGR gas flowing into the intake passage.

The above-described general formula enables accurate estimation of the flow rate of gas passing through the throttle portion, when the estimation is performed on the basis of an upstream pressure of the compressible fluid at a point immediately before the throttle portion and a downstream pressure of the compressible fluid at a point immediately after the throttle portion. However, in the present invention, the above-described, obtained upstream-side gas pressure is employed as the upstream pressure of the compressible fluid used in the general formula, and the above-described, obtained downstream-side gas pressure is employed as the downstream pressure of the compressible fluid used in the general formula.

Therefore, the provisional EGR gas flow rate obtained by the apparatus of the present invention involves an error caused by pipe friction. Thus, as described above, the apparatus of the present invention includes means for correcting such an error. As a result, the present apparatus can accurately estimate the flow rate of the EGR gas flowing into the intake passage, even when the difference between the obtained gas pressure on the upstream side of the throttle portion and the obtained gas pressure on the downstream side of the throttle portion becomes small (decreases), and therefore, there is a strong tendency that, rather than the degree of throttle, the pipe friction predominantly determines the EGR gas flow rate (i.e., when

change in the EGR gas flow rate stemming from throttle change decreases).

In this case, the upstream-gas-pressure obtaining means is preferably configured to obtain, as the upstream-side gas pressure, a pressure of gas in the exhaust passage to which the exhaust circulation pipe is connected, and the downstream-gas-pressure obtaining means is preferably configured to obtain, as the downstream-side gas pressure, a pressure of gas in the intake passage to which the exhaust circulation pipe is connected.

This configuration enables the upstream-side gas pressure and the downstream-side gas pressure to be obtained from, for example, outputs of an exhaust pressure sensor and an intake pressure sensor, respectively. Moreover, since the exhaust pressure is a value which can be accurately estimated through performance of a predetermined calculation, in a relatively easy manner as compared with, for example, the exhaust-circulation-pipe pressure, the exhaust pressure sensor can be omitted. The present invention enables accurate estimation of the EGR gas flow rate, even in the case where the respective pressures are obtained in the above-described manner.

In this case, the EGR-gas flow rate estimation means is preferably configured to calculate a correction value on the basis of the difference between the obtained upstream-side gas pressure and the obtained downstream-side gas pressure, and correct an error contained in the provisional EGR gas flow rate by use of the correction value.

In general, the differential pressure  $dP$  between the obtained upstream-side and downstream gas pressures has a strong correlation with the degree of influence of pipe friction on the gas flow rate. Specifically,

when the differential pressure  $dP$  is large, the degree of throttle is considered to predominantly determine the flow rate of the gas flowing through the throttle portion. In contrast, when the differential pressure  $dP$  is small, instead of the degree of throttle, pipe friction is considered to predominantly determine the gas flow rate. Therefore, the above-described configuration enables obtainment of a proper correction value, and thus the estimation accuracy of the EGR gas flow rate is improved.

In a more specific mode of the present invention, the provisional-EGR-gas-flow-rate estimation means is configured to estimate the provisional EGR gas flow rate  $G_{egr0}$  on the basis of the following general formula:

$$G_{egr0} = A_{egr} \cdot (2 \cdot P_{ex} \cdot \rho_a)^{1/2} \cdot \Phi$$

$$\Phi = ((\kappa/(\kappa-1)) \cdot ((P_b/P_{ex})^{2/\kappa} - (P_b/P_{ex})^{(1+1/\kappa)}))^{1/2}$$

where  $P_{ex}$  represents the obtained upstream-side gas pressure,  $P_b$  represents the obtained downstream-side gas pressure,  $A_{egr}$  represents an effective opening area of the throttle portion,  $\rho_a$  represents a density of EGR gas at an upstream point immediately before the throttle portion, and  $\kappa$  represents a specific heat ratio of EGR gas; and the EGR-gas flow rate estimation means is configured to obtain the correction value  $dP_{gain}$  in such a manner that the correction value increases toward 1 as the differential pressure ( $P_{ex} - P_b$ ) increases, and estimate the flow rate  $G_{egr}$  of EGR gas flowing into the intake passage, by multiplying the provisional EGR gas flow rate  $G_{egr0}$  by the correction value  $dP_{gain}$ .

## BRIEF DESCRIPTION OF THE DRAWINGS

Various other objects, features and many of the attendant advantages of the present invention will be readily appreciated as the same becomes better understood by reference to the following detailed description of the preferred embodiment when considered in connection with the accompanying drawings, in which:

FIG. 1 a schematic diagram showing the entire configuration of a system in which an engine control apparatus according to a first embodiment of the present invention is applied to a four-cylinder internal combustion engine (diesel engine);

FIG. 2A is a schematic cross-sectional view of the EGR control valve shown in FIG. 1;

FIG. 2B is a graph (table) showing the relation between drive signal applied to the EGR control valve and effective opening area;

FIG. 3 is a functional block diagram showing the contents of a program that a CPU shown in FIG. 1 executes;

FIG. 4 is an explanatory diagram showing values that the CPU shown in FIG. 1 calculates;

FIG. 5 is a functional block diagram showing the contents of a program that the CPU shown in FIG. 1 executes;

FIG. 6 is a diagram for explaining a general formula regarding gas flow rate at a throttle portion;

FIG. 7 is a functional block diagram showing the contents of a program that the CPU shown in FIG. 1 executes;

FIG. 8 is a graph showing actually measured values that were used to determine a function  $f_{Tex}$  which is a function for obtaining exhaust-circulation-pipe-inlet EGR-gas temperature  $T_{ex}$ ;



FIG. 9 is a graph showing actually measured values that were used to determine a function  $f_{Pex}$  which is a function for obtaining exhaust-manifold gas pressure  $P_{ex}$ ;

FIG. 10 is a graph showing the relation between cooling efficiency  $\eta_{egr}$  of an EGR-gas cooling apparatus and a value  $(G_{egr}/T_{ex})$  obtained by dividing EGR-gas flow rate  $G_{egr}$  by exhaust-circulation-pipe-inlet EGR-gas temperature  $T_{ex}$ ;

FIG. 11 is a graph showing actually measured values that were used to determine a function  $f_{\eta im}$  which is a function for obtaining intake-manifold heat transfer rate  $\eta_{im}$ ;

FIG. 12 is a flowchart showing a program that the CPU shown in FIG. 1 executes;

FIG. 13 is a table for determining an instruction fuel injection quantity, to which the CPU shown in FIG. 1 refers during execution of the program shown in FIG. 12;

FIG. 14 is a table for determining a base injection timing, to which the CPU shown in FIG. 1 refers during execution of the program shown in FIG. 12;

FIG. 15 is a table for determining an intake-manifold-outlet gas temperature reference value, to which the CPU shown in FIG. 1 refers during execution of the program shown in FIG. 12;

FIG. 16 is a table for determining an injection-timing correction value to which the CPU shown in FIG. 1 refers during execution of the program shown in FIG. 12;

FIG. 17 is a flowchart showing a program that the CPU shown in FIG. 1 executes;

FIG. 18 is a table to which the CPU of an engine control apparatus according to a modification of the first embodiment refers so as to determine a target EGR ratio;

FIG. 19 is a table to which the CPU shown in FIG. 1 refers so as to determine a target boost pressure; and

FIG. 20 is a graph showing the relation between cooling efficiency  $\eta_{egr}$  and EGR-gas flow rate  $G_{egr}$ , with exhaust-circulation-pipe-inlet EGR-gas temperature  $T_{ex}$  used as a parameter.

## DESCRIPTION OF THE PREFERRED EMBODIMENT

An embodiment of an control apparatus of an internal combustion engine (diesel engine) which incorporates an EGR-gas flow rate estimation apparatus according to the present invention, as well as an EGR control apparatus, will now be described with reference to the drawings.

FIG. 1 schematically shows the entire configuration of a system in which the engine control apparatus according to the present invention is applied to a four-cylinder internal combustion engine (diesel engine) 10. This system comprises an engine main body 20 including a fuel supply system; an intake system 30 for introducing gas to combustion chambers of individual cylinders of the engine main body 20; an exhaust system 40 for discharging exhaust gas from the engine main body 20; an EGR apparatus 50 for performing exhaust circulation; and an electric control apparatus 60.

Fuel injection valves 21 are disposed above the individual cylinders of the engine main body 20. The fuel injection valves 21 are electrically connected to the electric control apparatus 60. In response to a drive signal (an instruction signal corresponding to an instruction fuel injection

quantity  $q_{fin}$ ) from the electric control apparatus 60, each of the fuel injection valves 21 opens for a predetermined period of time, to thereby inject high-pressure fuel, which is supplied from an unillustrated fuel injection pump connected to a fuel tank.

The intake system 30 includes an intake manifold 31, which is connected to the respective combustion chambers of the individual cylinders of the engine main body 20; an intake pipe 32, which is connected to an upstream-side branching portion of the intake manifold 31 and constitutes an intake passage in cooperation with the intake manifold 31 (the intake manifold 31 and the intake pipe 32 may be collectively referred to as an "intake pipe"); a throttle valve 33, which is rotatably held within the intake pipe 32, and rotated by a throttle valve actuator 33a; an inter cooler 34, which is interposed in the intake pipe 32 to be located on the upstream side of the throttle valve 33; a compressor 35a of a turbocharger 35, which is interposed in the intake pipe 32 to be located on the upstream side of the inter cooler 34; and an air cleaner 36, which is disposed at a distal end portion of the intake pipe 32.

The exhaust system 40 includes an exhaust manifold 41, which is connected to the individual cylinders of the engine main body 20; an exhaust pipe 42, which is connected to a downstream-side merging portion of the exhaust manifold 41; a turbine 35b of the turbocharger 35 and a turbocharger throttle valve 35c, which are interposed in the exhaust pipe 42; and a diesel particulate filter (hereinafter referred to as "DPNR") 43, which is interposed in the exhaust pipe 42. The exhaust manifold 41 and the exhaust pipe 42 constitute an exhaust passage.

The turbocharger throttle valve 35c is connected to the electric

control apparatus 60. In response to a drive signal from the electric control apparatus 60, the turbocharger throttle valve 35c changes the cross-sectional area of an exhaust gas passage for exhaust gas flowing into the turbine 35b, to thereby change the effective capacity of the turbocharger 35. When the cross-sectional area of the exhaust gas passage is reduced through closure of the turbocharger throttle valve 35c, the boost pressure increases. In contrast, when the cross-sectional area of the exhaust gas passage is increased through opening of the turbocharger throttle valve 35c, the boost pressure decreases.

The DPNR 43 is a filter unit which accommodates a filter formed of a porous material such as cordierite and which collects, by means of a porous surface, the particulate matter contained in exhaust gas passing through the filter. In the DPNR 43, at least one metal element selected from alkaline metals such as potassium K, sodium Na, lithium Li, and cesium Cs; alkaline-earth metals such as barium Ba and calcium Ca; and rear-earth metals such as lanthanum La and yttrium Y is carried, together with platinum, on alumina serving as a carrier. Thus, the DPNR 43 also serves as a storage-reduction-type NO<sub>x</sub> catalyst unit which, after absorption of NO<sub>x</sub>, releases the absorbed NO<sub>x</sub> and reduces it.

The EGR apparatus 50 includes an exhaust circulation pipe 51, which forms a passage (EGR passage) for circulation of exhaust gas; an EGR control valve 52, which is interposed in the exhaust circulation pipe 51; and an EGR-gas cooling apparatus (EGR cooler) 53, which is interposed in the exhaust circulation pipe 51.

A portion of the exhaust circulation pipe 51 connected to an exhaust passage (the exhaust manifold 41) located on the upstream side of the

turbine 35b serves as an inlet for EGR gas (exhaust gas). A portion of the exhaust circulation pipe 51 connected to an intake passage (the intake manifold 31) located on the downstream side of the throttle valve 33 serves as an outlet for EGR gas. The exhaust circulation pipe 51 establishes communication between the inlet (exhaust circulation pipe inlet) and the outlet (exhaust circulation pipe outlet) to thereby form a gas flow pipe through which EGR gas flows from the inlet to the outlet.

When the intake manifold 31 is considered to be a gas flow pipe, its inlet is a connection portion between the intake manifold 31 and the exhaust circulation pipe 51, whereas the outlet of the intake manifold 31 is an intake air inflow portion extending toward the combustion chambers (openings to be opened and closed by intake valves) at which the intake manifold 31 is connected to the combustion chambers (cylinders) of the internal combustion engine 10.

As shown in FIG. 2A, the EGR control valve 52 includes a coil 52a, a valve member 52b, an opening 52c, etc. The valve member 52b and the opening 52c constitute a variable throttle portion whose degree of throttle can be changed. The coil 52a is connected to the electric control apparatus 60. The EGR control valve 52 is a duty-control-type solenoid valve designed in such a manner that in response to a drive signal (voltage signal having a duty ratio that changes in accordance with an EGR-control-valve opening instruction value  $SEGR$ ) from the electric control apparatus 60, the coil 52a changes the axial position (lift amount) of the valve member 52b. As shown in FIG. 2B, the EGR control valve 52 changes the effective opening area  $A_{egr}$  of the opening 52c in accordance with the EGR-control-valve opening instruction value  $SEGR$ , to thereby

adjust the quantity of exhaust gas to be circulated from the exhaust manifold 41 to the intake manifold 31 (exhaust-gas circulation quantity, EGR-gas flow rate).

The present apparatus employs a duty-control-type solenoid valve as the EGR control valve 52. However, other types of valves, such as a negative-pressure-drive-type valve designed to change the lift of a valve member by electrically controlling negative pressure and a step-motor-drive-type control valve may be used as the EGR control valve.

The EGR-gas cooling apparatus 53 has a passage formed therein for EGR gas which flows into the inlet of the apparatus and leaves from the outlet of the apparatus. Further, the EGR-gas cooling apparatus 53 has a cooling section exposed to the passage for EGR gas. Cooling water for the engine, which serves as a coolant, is caused to circulate through the cooling section.

The electric control apparatus 60 is a micro computer which includes a CPU 61, ROM 62, RAM 63, a backup RAM 64, an interface 65, etc., which are connected to one another by means of a bus. The ROM 62 stores a program to be executed by the CPU 61, tables (lookup tables, maps), constants, etc. The RAM 63 allows the CPU 61 to temporarily store data. The backup RAM 64 stores data in a state in which the power supply is on, and holds the stored data even after the power supply is shut off. The interface 65 contains AD converters.

The interface 65 is connected to a hot-wire-type air flow meter 71, disposed in the intake pipe 32; a new-air temperature sensor (intake temperature sensor) 72, provided in the intake passage between the inter cooler 34 and the throttle valve 33; an intake pressure sensor 73, disposed

in the intake passage to be located downstream of the throttle valve 33 and upstream of a point where the exhaust circulation pipe 51 is connected to the intake passage; an engine speed sensor 74; a water temperature sensor 75; and an accelerator opening sensor 76. The interface 65 receives respective signals from these sensors, and supplies the received signals to the CPU 61. Further, the interface 65 is connected to the fuel injection valves 21, the throttle valve actuator 33a, the turbocharger throttle valve 35c, and the EGR control valve 52; and outputs corresponding drive signals to these components in accordance with instructions from the CPU 61.

The hot-wire-type air flow meter 71 measures the mass flow rate of air (i.e., new air) that is newly taken into the intake pipe 32 via the air cleaner 36 (intake air quantity per unit time, new air quantity per unit time), and generates a signal (new-air flow rate)  $G_a$  corresponding to the mass flow rate of new air. The new-air temperature sensor 72 measures the temperature of new air that is taken into the intake pipe 32 via the air cleaner 36 (i.e., new-air temperature), and generates a signal  $T_a$  representing the new-air temperature.

The intake pressure sensor 73 generates a signal  $P_b$  representing the pressure (intake pressure, boost pressure) within the intake passage. That is, the intake pressure sensor 73 serves as intake-passage gas pressure obtaining means for obtaining, as intake-passage gas pressure, the pressure of gas in the intake passage (intake manifold 31) to which the exhaust circulation pipe 51 is connected. The intake pressure sensor 73 also serves downstream gas pressure obtaining means for obtaining, as downstream-side gas pressure, the gas pressure on the downstream side of the EGR control valve 52.

The engine speed sensor 74 detects the rotational speed of the engine 10, and generates a signal representing the engine speed NE. The engine speed sensor 74 also can detect the absolute crank angle of each cylinder. The water temperature sensor 75 detects the temperature of cooling water of the engine 10, and generates a signal THW representing the detected temperature. The accelerator opening sensor 76 detects the position of an accelerator pedal AP, and generates a signal Accp representing the accelerator opening (accelerator position).

Next, operation of the engine control apparatus having the above-described configuration will be described. The CPU 61 of the electric control apparatus 60 repeatedly executes, at predetermined intervals, a program for calculating various values, which program is shown in FIG. 3 in the form of a functional block diagram, to thereby calculate an actual EGR ratio Ract. Hereinafter, the program will be described on a block-by-block basis. Notably, some of values to be described below are shown in FIG. 4.

#### <Obtainment of Actual EGR ratio Ract>

The actual EGR ratio Ract is a value ( $Ract = Gegr/Gcyl$ ) obtained through division of an actual amount per unit time of EGR gas taken into a cylinder of the engine 10 (this is a mass flow rate of EGR gas actually flowing from the exhaust circulation pipe 51 to the intake passage, and is hereinafter referred to as "EGR-gas flow rate Gegr") by an actual amount per unit time of all gases taken into the cylinder (this is an actual all-gas mass flow rate, and is hereinafter referred to as "all-gas flow rate Gcyl"). The EGR-gas flow rate Gegr is equal to a value obtained by subtracting an



amount per unit time of new air taken into the cylinder (this is an air mass flow rate, and hereinafter is referred to as "actual new-air flow rate  $G_{aact}$ ") from the all-gas flow rate  $G_{cyl}$ . Accordingly, as shown in block B1, the CPU 61 calculates an actual EGR ratio  $R_{act}$  on the basis of the following Expression (1).

$$R_{act} = \frac{G_{cyl} - G_{aact}}{G_{cyl}} \quad \dots (1)$$

#### <Obtainment of Actual New-Air Flow Rate $G_{aact}$ >

The actual new-air flow rate  $G_{aact}$  used in Expression (1) changes with time delay with respect to a measured new-air flow rate  $G_a$  obtained through measurement by the air flow meter 71, and therefore is generally equal to a value obtained through performance of first-order lag processing for the measured new-air flow rate  $G_a$ . Accordingly, the CPU 61 calculates the actual new-air flow rate  $G_{aact}$  on the basis of the following Expression (2), which is shown in block B2 for performing the first-order lag processing for the measured new-air flow rate  $G_a$ .  $\alpha$  is a constant which assumes a value of 0 to 1. Notably,  $G_{aact}(n)$  represents an actual new-air flow rate  $G_{aact}$  obtained by the present calculation;  $G_{aact}(n-1)$  represents an actual new-air flow rate  $G_{aact}$  obtained by the previous calculation, which is performed a predetermined time earlier than the present calculation; and  $G_a(n)$  represents a measured new-air flow rate  $G_a$  on the basis of the output of the air flow meter 71 at the present calculation timing.

$$G_{aact}(n) = \alpha \cdot G_{aact}(n-1) + (1 - \alpha) \cdot G_a(n) \quad \dots (2)$$

#### <Obtainment of All-Gas Flow Rate Gcyl>

As can be inferred from the state equation of gas, the all-gas flow rate Gcyl, which is further necessary for performing the calculation of Expression (1), assumes a value corresponding to the pressure (intake pressure) Pb within the intake pipe downstream of the throttle valve 33 and the temperature (intake-gas temperature) Tbout of gas taken into the cylinder of the engine 10. Hereinafter, the temperature Tbout of gas taken into the cylinder of the engine 10 is referred to as "intake-manifold-outlet gas temperature Tbout."

In actuality, the all-gas flow rate Gcyl receives the influence of the quantity of gas remaining in the cylinder of the engine 10. Accordingly, as shown in block B3, the CPU 61 calculates the all-gas flow rate Gcyl on the basis of an empirically derived formula expressed by the following Expression (3). In Expression (3), a and b are matching constants determined experimentally, and Tbase represents an intake-manifold-outlet gas temperature (reference temperature) when the constants a and b were determined. The intake pressure (boost pressure) Pb used in Expression (3) is obtained from the intake pressure sensor 73.

$$G_{cyl} = \frac{T_{base}}{T_{bout}} (a \cdot P_b + b) \cdots (3)$$

#### <Obtainment of Actual Gas Temperature Tbout>

In order to perform the calculation of Expression (3), the

intake-manifold-outlet gas temperature  $T_{bout}$  must be obtained. As shown in block B4, the CPU 61 calculates the intake-manifold-outlet gas temperature  $T_{bout}$  in accordance with the following Expression (4).

$$T_{bout} = T_{bin} - \eta_{im} \cdot (T_{bin} - T_{wallim}) \quad \dots (4)$$

In Expression (4),

$T_{bin}$  represents the temperature of a mixture gas in a region within the intake manifold 31 on the outlet side of the EGR control valve 52; i.e., a region where EGR gas and new air are mixed (hereinafter, simply referred to as a "confluent portion" or an "intake-manifold inlet"), as shown in FIG. 4, and, hereinafter, the temperature of the mixture gas at the intake-manifold inlet is referred to as "intake-manifold-inlet gas temperature  $T_{bin}$ ";

$T_{wallim}$  represents the wall temperature of the intake manifold 31 extending from the intake-manifold inlet to a corresponding intake valve, and, hereinafter, the wall temperature is referred to as "intake-manifold wall temperature  $T_{wallim}$ "; and

$\eta_{im}$  represents the heat transfer rate (cooling efficiency) of the intake manifold 31 in a region extending between the intake-manifold inlet and the intake-manifold outlet (a portion to be opened and closed by the intake valve), and, hereinafter, the heat transfer rate is referred to as "intake-manifold heat transfer rate  $\eta_{im}$ ."

The above-described Expression (4) takes into consideration exchange of heat between the wall surface of the intake manifold 31 and gas taken into the cylinder, and exchange of heat between the wall surface of the intake manifold 31 and the outside air (air outside the intake manifold

31). These heat exchanges are represented by the second term ( $\eta_{im}$  ( $T_{bin} - T_{wallim}$ )) on the right side. This value ( $\eta_{im} (T_{bin} - T_{wallim})$ ) is a temperature change corresponding value which represents a change in temperature of intake air (new air + EGR gas) when the intake air passes through the intake manifold 31.

The heat exchange between the gas (intake air) and the gas flow pipe (intake manifold 31) has a strong correlation (for example, a proportional relation) with the difference between the temperature of the gas at the inlet and the wall temperature of the gas flow pipe. Further, the heat transfer rate can properly express the exchange of heat between the gas and the wall of the gas flow pipe and the exchange of heat between the wall of the gas flow pipe and the outside. Therefore, the above-described configuration enables simple and accurate estimation of the heat exchange, to thereby enable accurate estimation of the temperature change corresponding value.

Meanwhile, in order to obtain the intake-manifold-outlet gas temperature  $T_{bout}$  by use of Expression (4), the respective values ( $T_{bin}$ ,  $T_{wallim}$ ,  $\eta_{im}$ ) on the right side of Expression (4) must be obtained. Procedures for obtaining these values will be described on an individual basis.

#### <Obtainment of Intake-Manifold-Inlet Gas Temperature $T_{bin}$ >

As shown in block B5, the CPU 61 calculates the intake-manifold-inlet gas temperature  $T_{bin}$  in accordance with the following Expression (5), which is based on the law of energy conservation.

$$T_{bin} = (G_{aact} \cdot T_a \cdot C_{air} + G_{egr} \cdot T_{egr} \cdot C_{egr}) / (G_{all} \cdot C_{ave}) \quad \dots (5)$$

Respective values on the right side of Expression (5) will be described with reference to FIG. 4.

$G_{aact}$  represents the previously-described actual new-air flow rate, which is obtained by the above-described block B2 in accordance with Expression (2).

$T_a$  represents the previously-described new-air temperature, which is detected by the new-air temperature sensor 72.

$C_{air}$  represents the specific heat of new air (new-air specific heat), which is a constant that is previously given.

$G_{egr}$  represents the previously-described EGR-gas flow rate, which is obtained by a method described below.

$T_{egr}$  represents the EGR-gas temperature immediately before EGR gas and new air are mixed at the confluent portion. Specifically, the temperature  $T_{egr}$  is the temperature of EGR gas at an EGR gas outlet, which is a connection portion of the exhaust circulation pipe 51 through which the exhaust circulation pipe is connected to the intake passage, and is hereinafter referred to as "exhaust-circulation-pipe-outlet EGR-gas temperature (EGR-passage-outlet EGR-gas temperature)  $T_{egr}$ ." The exhaust-circulation-pipe-outlet EGR-gas temperature  $T_{egr}$  is obtained by a method described below.

$C_{egr}$  represents the specific heat of EGR gas (EGR-gas specific heat), which is a constant that is previously given.

$G_{all}$  represents the total quantity of the mixture of EGR gas and new air; i.e., the sum of the actual new-air flow rate  $G_{aact}$  and the EGR-gas flow

rate  $G_{egr}$ , and is hereinafter referred to as "intake-manifold-inlet gas flow rate  $G_{all}$ ."

$C_{ave}$  represents the specific heat (mixture gas specific heat) of the mixture of EGR gas and new air, which is a constant that is previously given.

In order to obtain the intake-manifold-inlet gas temperature  $T_{bin}$  by use of Expression (5), the exhaust-circulation-pipe-outlet EGR-gas temperature  $T_{egr}$ , the EGR-gas flow rate  $G_{egr}$ , and the intake-manifold-inlet gas flow rate  $G_{all}$  must be obtained. Procedures for obtaining these values will be described on an individual basis.

#### <Obtainment of Exhaust-Circulation-Pipe-Outlet EGR-Gas Temperature $T_{egr}$ >

As shown in block B6, the CPU 61 calculates the exhaust-circulation-pipe-outlet EGR-gas temperature  $T_{egr}$  in accordance with the following Expression (6). Block B6 serves as an outlet EGR-gas temperature estimating means.

$$T_{egr} = T_{ex} - \eta_{egr} \cdot (T_{ex} - T_{HW}) \quad \dots(6)$$

In Expression (6),

$T_{ex}$  represents the EGR-gas temperature at the inlet of the exhaust circulation pipe 51 in the vicinity of the connection portion between the exhaust circulation pipe 51 and the exhaust manifold 41 (i.e., exhaust gas temperature in the vicinity of the connection portion between the exhaust

manifold 41 and the exhaust circulation pipe 51), and is hereinafter referred to as "exhaust-circulation-pipe-inlet EGR-gas temperature (EGR-passage-inlet EGR-gas temperature)  $T_{ex}$ ";

$\eta_{egr}$  represents the cooling efficiency (heat transfer rate) of the EGR-gas cooling apparatus 53; and

$T_{HW}$  represents the temperature of cooling water of the engine 10, which is equal to the temperature  $T_{reibai}$  of coolant, because the coolant of the EGR-gas cooling apparatus 53 is the cooling water of the engine.

The above-described Expression (6) takes into consideration exchange of heat between the EGR-gas cooling apparatus 53 (the cooling section thereof) and EGR gas flowing through the EGR-gas cooling apparatus 53. That is, the second term ( $\eta_{egr} (T_{ex} - T_{HW})$ ) on the right side of Expression (6) is a temperature change corresponding value which represents a change in temperature of EGR gas when the EGR gas flows through the EGR-gas cooling apparatus 53.

In actuality, exchange of heat occurs between every portion of EGR gas and the wall surface of the exhaust circulation pipe 51 during a period between a point in time when that portion of the EGR gas flows into the inlet of the exhaust circulation pipe 51 and a point in time when that portion of the EGR gas reaches the outlet of the exhaust circulation pipe 51.

However, the quantity of heat exchanged between the EGR gas and the wall surface of the exhaust circulation pipe 51 is considerably small as compared with the quantity of heat exchanged between the EGR gas and the EGR-gas cooling apparatus 53. Accordingly, the second term ( $\eta_{egr} (T_{ex} - T_{HW})$ ) on the right side of Expression (6) is substantially equal to a value that represents a change in temperature of EGR gas during a period between

entrance to the inlet of the exhaust circulation pipe 51 and arrival at the outlet of the exhaust circulation pipe 51.

Meanwhile, in order to obtain the exhaust-circulation-pipe-outlet EGR-gas temperature  $T_{egr}$  by use of Expression (6), the above-described exhaust-circulation-pipe-inlet EGR-gas temperature  $T_{ex}$  and the above-described cooling efficiency  $\eta_{egr}$  of the EGR-gas cooling apparatus must be obtained. Procedures for obtaining these values will be described on an individual basis.

#### <Obtainment of Exhaust-Circulation-Pipe-Inlet EGR-Gas Temperature $T_{ex}$ >

As shown in blocks B8 and B9, the CPU 61 calculates the exhaust-circulation-pipe-inlet EGR-gas temperature  $T_{ex}$  (exhaust gas temperature  $T_{ex}$ ) in accordance with the following Expression (7). Blocks B8 and B9 serve as an EGR-gas temperature obtaining means.

$$T_{ex} = f_{Tex}(X_{Tex}) \quad \dots (7)$$

$$X_{Tex} = G_f^a / G_{aact}$$

$$\text{or} \quad X_{Tex} = (G_f^a / G_{aact}) (P_b / P_{ex})$$

$$\text{or} \quad X_{Tex} = G_f \Phi$$

$$\text{or} \quad X_{Tex} = G_f \Phi (P_b / P_{ex})$$

$$\Phi = G_f / G_a$$

where

$G_f$ : fuel injection quantity per unit time (g/s)

$G_{aact}$ : actual new-air flow rate (g/s)



$P_b$ : boost pressure

$P_{ex}$ : exhaust manifold gas pressure

$\Phi$ : equivalent ratio

$a$ : constant

In Expression (7),

the fuel injection quantity per unit time  $G_f$  can be obtained on the basis of instruction fuel injection quantity  $q_{fin}$  and engine speed  $NE$ , as shown in block BP3 of FIG. 5 (e.g.,  $G_f = k_{Gf} \cdot q_{fin} \cdot NE$  ( $k_{Gf}$ : constant));

the actual new-air flow rate  $G_{aact}$  is obtained by the above-described block B2 on the basis of Expression (2);

the boost pressure  $P_b$  is the intake pressure  $P_b$ , and is obtained from the intake pressure sensor 73; and

the exhaust manifold gas pressure  $P_{ex}$  (the pressure of EGR gas at the EGR gas inlet, which is a connection portion between the exhaust circulation pipe 51 and the exhaust passage formed by the exhaust manifold 41) is obtained by a method described below.

The above-described Expression (7) is based on the finding that "the exhaust-circulation-pipe-inlet EGR-gas temperature  $T_{ex}$  greatly depends on energy supplied to a cylinder (heat generation amount), and transfer of heat generated within the cylinder to the gas." The energy supplied to the cylinder has a strong correlation with the fuel injection quantity  $G_f$ . Further, the transfer of heat generated within the cylinder to the gas has a strong correlation with the actual new-air flow rate  $G_{aact}$  (the actual new-air flow rate  $G_{aact}$  does not contribute to heat generation, but functions to decrease the exhaust gas temperature), or the equivalent ratio  $\Phi$ , which is a value

relating to the gas specific heat. Therefore, in Expression (7), the above-described values are selectively used for the variable  $X_{Tex}$ .

Notably, the value (boost pressure  $P_b$ /exhaust manifold gas pressure  $P_{ex}$ ), which is one value used for the variable  $X_{Tex}$ , represents the easiness of passage of exhaust gas through the exhaust manifold 41 (the easiness of remaining within the exhaust manifold 41). The longer the time during which the exhaust gas remains within the exhaust manifold 41, the greater the quantify of heat transferred between the exhaust gas and the outside of the exhaust manifold 41. Accordingly, through introduction of (boost pressure  $P_b$ /exhaust manifold gas pressure  $P_{ex}$ ) as a parameter, estimation accuracy of the exhaust-circulation-pipe-inlet EGR-gas temperature  $T_{ex}$  is improved. Further, the boost pressure  $P_b$  has a correlation with the EGR gas quantity, and when the EGR gas quantity increases, the temperature at the time of start of combustion increases, and the exhaust gas temperature  $T_{ex}$  (exhaust-circulation-pipe-inlet EGR-gas temperature  $T_{ex}$ ) increases accordingly. From this point of view, employment of the boost pressure  $P_b$  as a parameter contributes to improving the estimation accuracy of the exhaust gas temperature  $T_{ex}$ .

The function  $f_{Tex}$  and the constant  $a$  in Expression (7) are determined for each engine model. The following is an example procedure of determining the function  $f_{Tex}$  and the constant  $a$ .

(Step 1) Operation conditions of an engine, for which the function  $f_{Tex}$  and the constant  $a$  are to be determined, are changed; and necessary engine state quantities ( $G_f$ ,  $G_{aact}$ ,  $P_b$ ,  $P_{ex}$ ,  $T_{ex}$ ) are measured.

(Step 2) On the basis of measurement results, the constant  $a$  is determined in such a manner that the variable  $X_{Tex}$  and an actually

measured value of the EGR-gas temperature  $T_{ex}$  exhibit close correlation. Notably, when a value containing the equivalent ratio  $\Phi$  is employed as the variable  $X_{Tex}$ , the adjustment (determination) of the value of the constant  $a$  is omitted.

(Step 3) The function  $f_{Tex}$  is determined on the basis of the variable  $X_{Tex}$  determined in accordance with the determined constant  $a$ , as well as the actually measured value of the EGR-gas temperature  $T_{ex}$ .

FIG. 8 shows an example of the relation between the variable  $X_{Tex}$  and the actually measured exhaust-circulation-pipe-inlet EGR-gas temperature  $T_{ex}$  for the case where  $G_f \cdot \Phi \cdot (P_b/P_{ex})$  is selected as the variable  $X_{Tex}$ . In this case, the function  $f_{Tex}$  was determined as follows.

$$T_{ex} = f_{Tex}(X_{Tex}) = 545.9 \cdot X_{Tex}^{0.3489}$$

#### <Obtainment of Exhaust Manifold Gas Pressure $P_{ex}$ >

In the case where a variable containing the exhaust manifold gas pressure  $P_{ex}$  is used as the variable  $X_{Tex}$  of the above-described Expression (7), the exhaust manifold gas pressure  $P_{ex}$  must be obtained. As shown in FIG. 5, which is a functional block diagram, the CPU 61 calculates the exhaust manifold gas pressure  $P_{ex}$  in accordance with the following Expression (8). Notably, the exhaust manifold gas pressure (exhaust-circulation-pipe-inlet EGR gas pressure)  $P_{ex}$  is the pressure  $P_{ex}$  of EGR gas at the EGR gas inlet, which is a connection portion between the exhaust circulation pipe 51 and the exhaust passage formed by the exhaust manifold 41. Further, the functional blocks shown in FIG. 5 serves exhaust-circulation-pipe-inlet EGR gas pressure obtaining means for obtaining the pressure of EGR gas at the exhaust passage (EGR-gas-inlet

EGR gas pressure obtaining means, exhaust pressure obtaining means), or upstream gas pressure obtaining means for obtaining, as upstream-side gas pressure, the gas pressure on the upstream side of the EGR control valve 52.

$$\left. \begin{aligned} P_{ex} &= f_{Pex}(X_{Pex}) \\ X_{Pex} &= (G_f + G_{aact}) \cdot P_b / K_{vn} \\ K_{vn} &= A_{vn} + a_{vn} \end{aligned} \right\} \dots(8)$$

where

$G_f$ : fuel injection quantity per unit time (g/s)

$G_{aact}$ : actual new-air flow rate (g/s)

$P_b$ : boost pressure

$K_{vn}$ : throttle coefficient of the variable capacity turbocharger

$A_{vn}$ : opening of the variable capacity turbocharger (0 - 100%)

$a_{vn}$ : positive constant

In Expression (8),

the fuel injection quantity  $G_f$  is obtained on the basis of instruction fuel injection quantity  $q_{fin}$  and engine speed  $NE$ , as shown in block BP3 of FIG. 5;

the actual new-air flow rate  $G_{aact}$  is obtained by the above-described block B2 on the basis of Expression (2);

the boost pressure  $P_b$  is the intake pressure  $P_b$ , and is obtained from the intake pressure sensor 73; and

the opening  $A_{vn}$  of the variable capacity turbocharger is a value

determined with reference to a table, as shown in block BP4 of FIG. 5, where the instruction fuel injection quantity  $q_{fin}$  and the engine speed  $NE$  are used as arguments.

The CPU 61 supplies a drive signal to the turbocharger throttle value 35c in such a manner that the opening of the turbocharger throttle value 35c corresponds to the value  $Avn$ . Further, in block BP5, the constant  $avn$  is added to the opening  $Avn$  of the variable capacity turbocharger, whereby the opening  $Avn$  is converted to the variable-capacity-turbocharger throttle coefficient  $Kvn$  of Expression (8). Notably, as will be described later, a target boost pressure may be set, and the value  $Avn$  may be determined in such a manner that the actual boost pressure becomes equal to the target boost pressure.

The above-described Expression (8) is based on the finding that "the exhaust manifold gas pressure  $P_{ex}$  has a strong correlation with the quantity of gas flowing into the cylinder ( $G_{aact} + G_f$ ), the opening  $Avn$  of the turbocharger throttle value 35c, and the boost pressure, which represents the resistance of the turbine 35b of the turbocharger 35."

The function  $fP_{ex}$  and the constant  $avn$  in Expression (8) are determined for each engine model. The following is an example procedure for determining the function  $fP_{ex}$  and the constant  $avn$ .

(Step 1) Operation conditions of an engine, for which the function  $fP_{ex}$  and the constant  $avn$  are to be determined, are changed; and necessary engine state quantities ( $G_f$ ,  $G_{aact}$ ,  $P_b$ ,  $Avn$ ,  $P_{ex}$ ) are measured.

(Step 2) On the basis of measurement results, the constant  $avn$  is determined in such a manner that the variable  $XP_{ex}$  and the exhaust manifold gas pressure  $P_{ex}$  exhibit close correlation.

(Step 3) The function  $f_{Pex}$  is determined on the basis of the variable  $X_{Pex}$  determined in accordance with the determined constant  $av_n$ , as well as the actually measured value of the exhaust manifold gas pressure  $P_{ex}$ .

FIG. 9 shows measurement values which were used to determine the function  $f_{Pex}$  in the above-described manner. In this case, the function  $f_{Pex}$  was determined as represented by the following Expression (9). As described above, in the present embodiment, the exhaust pressure  $P_{ex}$  can be obtained without use of an exhaust pressure sensor, whereby cost of the apparatus can be reduced.

$$P_{ex} = f_{Pex}(X_{Pex}) = -2 \cdot 10^{-8} \cdot X_{Pex}^2 + 0.059 \cdot X_{Pex} + 100.59 \quad \cdots (9)$$

Through the above-described procedure, the various values ( $G_f$ ,  $G_{aact}$ ,  $P_b$ ,  $P_{ex}$ ) necessary for obtaining the variable  $X_{Tex}$  of Expression (7) are obtained, and the variable  $X_{Tex}$  is determined. Accordingly, the CPU 61 obtains the exhaust-circulation-pipe-inlet EGR-gas temperature  $T_{ex}$  (exhaust gas temperature  $T_{ex}$ ) by performing calculation in accordance with Expression (7). Meanwhile, in order to obtain the exhaust-circulation-pipe-outlet EGR-gas temperature  $T_{egr}$  by use of Expression (6), the cooling efficiency  $\eta_{egr}$  of the EGR-gas cooling apparatus must be further obtained.

#### <Obtainment of Cooling Efficiency $\eta_{egr}$ of EGR-Gas Cooling Apparatus>

As shown in block B10 of FIG. 3, the CPU 61 calculates the cooling efficiency  $\eta_{egr}$  of the EGR-gas cooling apparatus in accordance with the

following Expression (10). Block B10 serves as a cooling-apparatus cooling efficiency obtaining means (estimation means).

$$\eta_{egr} = f \eta_{egr}(G_{egr}/T_{ex}) \quad \cdots(10)$$

As shown in Expression (10), in order to obtain the cooling efficiency  $\eta_{egr}$  of the EGR-gas cooling apparatus, the above-described exhaust-circulation-pipe-inlet EGR-gas temperature  $T_{ex}$  and EGR-gas flow rate  $G_{egr}$  must be obtained. The exhaust-circulation-pipe-inlet EGR-gas temperature  $T_{ex}$  is obtained by blocks B8 and B9 in accordance with the above-described Expression (7). The EGR-gas flow rate  $G_{egr}$  is obtained by block B12, which will be described later.

Notably, a value (EGR-gas flow rate corresponding value) corresponding to the EGR-gas flow rate  $G_{egr}$  may be used as the EGR-gas flow rate  $G_{egr}$  in Expression (10). For example, the EGR-gas flow rate  $G_{egr}$  may be replaced with EGR-gas flow velocity  $V_{egr}$  at a predetermined location of the exhaust circulation pipe 51. Since the shape of the EGR passage (the EGR passage formed by the exhaust circulation pipe 51 and the EGR-gas cooling apparatus 53) is known, the EGR-gas flow rate  $G_{egr}$  can be estimated on the basis of the EGR-gas flow velocity  $V_{egr}$ . This is the reason why the EGR-gas flow rate  $G_{egr}$  can be replaced with the EGR-gas flow velocity  $V_{egr}$ . The EGR-gas flow velocity  $V_{egr}$  may be obtained directly from a flow velocity sensor disposed within the exhaust circulation pipe 51.

The function  $f\eta_{egr}$  in Expression (10) is determined for each engine model. The following is an example procedure for determining the function

$f_{\eta_{egr}}$ .

(Step 1) Operation conditions of an engine, for which the function  $f_{\eta_{egr}}$  is to be determined, are changed; and necessary engine state quantities ( $G_{egr}$ ,  $T_{ex}$ ,  $\eta_{egr}$ ) are measured.

(Step 2) On the basis of measurement results, the relation between  $\eta_{egr}$  and  $G_{egr}/T_{ex}$  is determined in the form of a graph, as shown in FIG. 10.

(Step 3) The function  $f_{\eta_{egr}}$  is determined on the basis of the graph prepared in Step 2.

As shown in FIG. 20, the relation between the cooling efficiency  $\eta_{egr}$  and the EGR-gas flow rate  $G_{egr}$  changes as the exhaust-circulation-pipe-inlet EGR-gas temperature  $T_{ex}$  changes. In contrast, as shown in FIG. 10, the relation between the cooling efficiency  $\eta_{egr}$  and the value ( $= G_{egr}/T_{ex}$ ) obtained by dividing the EGR-gas flow rate  $G_{egr}$  by the exhaust-circulation-pipe-inlet EGR-gas temperature  $T_{ex}$  is univocally determined, irrespective of the exhaust-circulation-pipe-inlet EGR-gas temperature  $T_{ex}$ . In other words, since an experiment revealed that the cooling efficiency  $\eta_{egr}$  is generally in inverse proportion to the exhaust-circulation-pipe-inlet EGR-gas temperature  $T_{ex}$ , the function  $f_{\eta_{egr}}$  can be simply obtained by obtaining the cooling efficiency  $\eta_{egr}$  while using the value ( $G_{egr}/T_{ex}$ ) as a variable.

In the present apparatus, the above-described function  $f_{\eta_{egr}}$  is stored in the ROM 62 in the form of a function, or data consisting of combinations of values of  $G_{egr}/T_{ex}$  and  $\eta_{egr}$  are stored in the ROM 62 in the form of values of a table (single-dimensional map); and an actually-obtained cooling efficiency  $\eta_{egr}$  is obtained on the basis of an actual value of  $G_{egr}/T_{ex}$  and the stored function or table.



Notably, when the electric control apparatus 60 has surplus calculation capability and/or storage capacity, there may be employed a method such that values of  $G_{egr}$ ,  $T_{ex}$ , and  $\eta_{egr}$  are measured, while operating conditions of the engine are changed; the measured data are stored in the ROM 62 in the form of a table  $Map_{\eta_{egr}}$  (two-dimensional map); and an actual cooling efficiency  $\eta_{egr}$  is obtained on the basis of an actual EGR-gas flow rate  $G_{egr}$ , an actual exhaust-circulation-pipe-inlet EGR-gas temperature  $T_{ex}$ , and the stored table  $Map_{\eta_{egr}}$ . Alternatively, there may be employed a method such that a function  $g_{Tex}(G_{egr})$  for determining the cooling efficiency  $\eta_{egr}$  from the EGR-gas flow rate  $G_{egr}$  is obtained and stored in the ROM for each exhaust-circulation-pipe-inlet EGR-gas temperature  $T_{ex}$ ; a proper function  $g_{Tex}$  is selected from the plurality of stored functions  $g_{Tex}$  on the basis of an actual exhaust-circulation-pipe-inlet EGR-gas temperature  $T_{ex}$ ; and an actual cooling efficiency  $\eta_{egr}$  is obtained from the selected function  $g_{Tex}$  and an actual EGR-gas flow rate  $G_{egr}$ .

Through the above-described procedure, the exhaust-circulation-pipe-inlet EGR-gas temperature  $T_{ex}$ , the cooling efficiency  $\eta_{egr}$  of the EGR-gas cooling apparatus, and the cooling water temperature THW (coolant temperature  $T_{reibai}$ ), which are necessary for the calculation performed by block B6 in accordance with Expression (6), are obtained. Therefore, the CPU 61 can obtain the exhaust-circulation-pipe-outlet EGR-gas temperature  $T_{egr}$  by use of Expression (6). At this stage, the above-described EGR-gas flow rate  $G_{egr}$  and intake-manifold-inlet gas flow rate  $G_{all}$ , which are variables, are required for performing the calculation of Expression (5). The methods for obtaining these values will now be described.

#### <Obtainment of EGR-Gas Flow Rate Gegr>

The above-described EGR control valve 52 forms a variable throttle portion by the valve member 52b and the opening 52c, and the EGR gas passes through the throttle portion. The flow rate Gegr0 of EGR gas passing through the throttle portion, as measured downstream of the throttle portion, can be obtained by the following Expression (11). Expression (11) is a general formula regarding flow rate of a compressible fluid, which is valid insofar as the flow velocity at the throttle portion does not exceed sonic velocity. Since the flow velocity at the throttle portion 52c of the EGR control valve 52 does not exceed sonic velocity, Expression (11) is valid.

$$\begin{aligned} G_{egr0} &= A_{egr} \cdot \sqrt{2 \cdot P_{up} \cdot \rho_a} \cdot \Phi \\ \Phi &= \sqrt{\frac{\kappa}{\kappa-1} \cdot \left\{ \left( \frac{P_{dn}}{P_{up}} \right)^{\frac{2}{\kappa}} - \left( \frac{P_{dn}}{P_{up}} \right)^{\left(1+\frac{1}{\kappa}\right)} \right\}} \end{aligned} \quad \left. \vphantom{\begin{aligned} G_{egr0} &= A_{egr} \cdot \sqrt{2 \cdot P_{up} \cdot \rho_a} \cdot \Phi \\ \Phi &= \sqrt{\frac{\kappa}{\kappa-1} \cdot \left\{ \left( \frac{P_{dn}}{P_{up}} \right)^{\frac{2}{\kappa}} - \left( \frac{P_{dn}}{P_{up}} \right)^{\left(1+\frac{1}{\kappa}\right)} \right\}} \right\}} \right\} \dots(11)$$

The values used in Expression (11) will be described with reference to FIG. 6.

$P_{up}$  represents the upstream-side pressure at a position immediately before the throttle portion.

$P_{dn}$  represents the downstream-side pressure at a position immediately after the throttle portion.

$\rho_a$  represents the density of EGR gas on the upstream side of the throttle portion.

$\kappa$  represents the specific heat ratio of EGR gas.

$A_{egr}$  represents the effective opening area of the throttle portion

(throttle portion formed by the valve member 25b and the opening 52c of the EGR control valve 52).

In actuality, the CPU 61 employs the exhaust manifold gas pressure  $P_{ex}$  as the upstream-side pressure  $P_{up}$ , and the intake pressure (boost pressure)  $P_b$  as the downstream-side pressure  $P_{dn}$ ; and obtains the EGR gas flow rate  $G_{grO}$  at a downstream position immediately after the throttle portion formed by the valve member 25b and the opening 52c of the EGR control valve 52, on the basis of the following Expression (12). For the sake of convenience, this EGR gas flow rate  $G_{grO}$  is called a provisional EGR gas flow rate  $G_{grO}$ .

$$\left. \begin{aligned} G_{grO} &= f_{G_{gr}}(P_{ex}, P_b, A_{egr}) \\ &= A_{egr} \cdot \sqrt{2 \cdot P_{ex} \cdot \rho_a} \cdot \Phi \\ \Phi &= \sqrt{\frac{\kappa}{\kappa-1} \cdot \left\{ \left( \frac{P_b}{P_{ex}} \right)^{\frac{2}{\kappa}} - \left( \frac{P_b}{P_{ex}} \right)^{\left(1+\frac{1}{\kappa}\right)} \right\}} \end{aligned} \right\} \dots(12)$$

The exhaust manifold gas pressure  $P_{ex}$  in Expression (12) is obtained by block BP1 of FIG. 5 in accordance with the above-described Expression (8) (in actuality, Expression (9)).

The boost pressure  $P_b$  is obtained from the intake pressure sensor 73.

The specific heat ratio  $\kappa$  of EGR gas is given in advance.

The effective opening area  $A_{egr}$  is obtained on the basis of the EGR-control-valve opening instruction value  $SEGR$ , which is an instruction value supplied from the CPU 61 to the EGR control valve 52, and a table

MapAegr shown in FIG. 2B and stored in the ROM 62. In this case, the effective opening area Aegr may be obtained on the basis of the table MapAegr and a signal from a sensor for detecting the lift of the EGR control valve 52, without use of the EGR-control-valve opening instruction value SEGR.

The upstream-side density  $\rho_a$  is obtained on the basis of the exhaust manifold gas pressure  $P_{ex}$ , the EGR gas temperature  $T_{ex}$  at the inlet of the exhaust circulation pipe 51, and the state equation of gas. In actuality, the EGR gas is cooled by the EGR-gas cooling apparatus 53, and thus, the temperature of the EGR gas drops. However, since the pressure of the EGR gas also drops, the density obtained in the manner as described is substantially equal to the density of EGR gas flowing into the EGR control valve 52.

However, the EGR gas flow rate  $G_{egr0}$  obtained in the manner as described is sometimes of poor accuracy, because of pipe friction produced between the EGR gas and the EGR passage (passage formed by the exhaust circulation pipe 51 and the EGR-gas cooling apparatus 53).

That is, in the above-described Expression (11) the exhaust manifold gas pressure  $P_{ex}$  is employed as the upstream-side pressure  $P_{up}$ , and the intake pressure (boost pressure)  $P_b$  is employed as the downstream-side pressure  $P_{dn}$ . Therefore, the above-described Expression (12) is valid in a state in which a change in throttle (i.e., the effective opening area Aegr) predominantly determines the flow rate of gas passing through the throttle portion. However, the above-described Expression (12) is not always valid in other states; i.e., a state in which pipe friction predominantly determines the gas flow rate.

Whether the throttle (the degree of throttle) or the pipe friction predominantly determines the gas flow rate should be determined in accordance with the relation between the effective opening area  $A_{egr}$  of the throttle and the differential pressure  $dP$  between the exhaust manifold gas pressure  $P_{ex}$  and the intake pressure  $P_b$ . However, in general, when the differential pressure  $dP (= P_{ex} - P_b)$  is large, the throttle (the degree of throttle) is considered to predominantly determine the gas flow rate. In contrast, when the differential pressure  $dP$  is small, instead of throttle change, pipe friction, which changes in accordance the length of the exhaust circulation pipe 51, is considered to predominantly determine the gas flow rate, because of employment of the exhaust manifold gas pressure  $P_{ex}$  and the intake pressure  $P_b$  as the upstream-side pressure  $P_{up}$  and the downstream-side pressure  $P_{dn}$ , respectively.

Moreover, as a result of employment, in the above-described Expression (11), of the exhaust manifold gas pressure  $P_{ex}$  and the intake pressure (boost pressure)  $P_b$  as the upstream-side pressure  $P_{up}$  and the downstream-side pressure  $P_{dn}$ , respectively, the differential pressure  $dp$  used in the calculation becomes greater than the differential pressure actually produced across the throttle portion (the differential pressure between points immediately before and after the throttle portion). Therefore, in a region where the differential pressure  $dp$  is small, the differential pressure produced across the throttle portion is extremely small, and the throttle does not serve as a predominant factor of the gas flow rate. Therefore, the provisional EGR gas flow rate  $G_{egr0}$  obtained by Expression (12) tends to be calculated as a value greater than the actual flow rate of EGR gas passing through the EGR control valve 52.

In view of the foregoing, the present apparatus introduces a correction coefficient (correction value)  $dP_{gain}$  which is determined in accordance with the differential pressure  $dP$  ( $= P_{ex} - P_b$ ) between the exhaust manifold gas pressure  $P_{ex}$  and the intake pressure (boost pressure)  $P_b$ , and corrects the EGR gas flow rate  $G_{egr0}$ , obtained by the above-described Expression (12), by use of the correction coefficient  $dP_{gain}$ .

That is, since the influence of the pipe friction on the EGR gas flow rate increases as the differential pressure  $dP$  decreases, the present apparatus obtains the exhaust-circulation-pipe-outlet EGR-gas flow rate  $G_{egr}$  by multiplying the EGR gas flow rate  $G_{egr0}$ , obtained by the above-described Expression (12), by the correction coefficient  $dP_{gain}$ , which approaches "0" as the differential pressure  $dP$  decreases, and approaches "1" as the differential pressure  $dP$  increases.

Specifically, the CPU 61 obtains the correction coefficient (correction value)  $dP_{gain}$  by block BG1 shown in FIG. 7, on the basis of the differential pressure  $dP$  and a table  $Map_{dP_{gain}}$  stored in the ROM 62 and shown in block BG1. Further, the CPU 61 obtains the effective opening area  $A_{egr}$  by block B12a shown in FIG. 3, on the basis of the EGR-control-valve opening instruction value  $SEGR$  and the table  $Map_{A_{egr}}$  shown in FIG. 2B and stored in the ROM 62. Subsequently, the CPU 61 obtains the exhaust-circulation-pipe-outlet EGR-gas flow rate  $G_{egr}$  (flow rate of EGR gas actually passing through the EGR control valve 52) by block B12 shown in FIG. 3 on the basis of the above-described Expression (12) and the following Expression (13).

$$\begin{aligned} \text{Gegr} &= \text{dPgain} \cdot \text{fGegr}(\text{Pex}, \text{Pb}, \text{Aegr}) \\ &= \text{dPgain} \cdot \text{Gegr0} \end{aligned} \quad \dots(13)$$

Notably, a portion of block B12 which executes the above-described Expression (12) serves as provisional-EGR-gas-flow-rate estimation means for obtaining, as a provisional EGR gas flow rate Gegr0, the flow rate of EGR gas passing through the EGR control valve, by use of a general formula (the above-described Expression (11)) in which the flow rate of a compressible fluid passing through a throttle portion is represented on the basis of an upstream pressure of the compressible fluid at a point immediately before the throttle portion and a downstream pressure of the compressible fluid at a point immediately after the throttle portion, wherein the above-described, obtained upstream-side gas pressure is employed as the upstream pressure of the compressible fluid at a point immediately before the throttle portion, and the above-described, obtained downstream-side gas pressure is employed as the downstream pressure of the compressible fluid at a point immediately after the throttle portion.

Further, a portion of block B12 which obtains the correction coefficient (correction value) dPgain and a portion of block B12 which executes Expression (13) in order to multiply the provisional EGR gas flow rate by the correction coefficient dPgain, to thereby correct the provisional EGR gas flow rate Gegr0, serves as EGR-gas-flow-rate estimation means for estimating the flow rate Gegr of EGR gas flowing from the exhaust circulation pipe 51 to the intake passage, by correcting an error which is contained in the estimated provisional EGR gas flow rate Gegr0 and which

is caused by the pipe friction between the exhaust circulation pipe 51 and the EGR gas.

<Obtainment of Intake-Manifold-Inlet Gas Flow Rate  $G_{all}$ >

As described above, the intake-manifold-inlet gas flow rate  $G_{all}$  is the sum of the actual new-air flow rate  $G_{aact}$  and the EGR-gas flow rate  $G_{egr}$ . As shown in block B13 of FIG. 3, the CPU 61 calculates the intake-manifold-inlet gas flow rate  $G_{all}$  in accordance with the following Expression (14).

$$G_{all} = G_{aact} + G_{egr} \quad \dots(14)$$

The actual new-air flow rate  $G_{aact}$  in expression (14) is obtained by block B2 on the basis of the above-described Expression (2). The EGR-gas flow rate  $G_{egr}$  is obtained by block B12 on the basis of the above-described Expressions (12) and (13).

Through the above-described procedure, the various values required for performing the calculation of Expression (5) are obtained. Accordingly, the CPU 61 obtains the intake-manifold-inlet gas temperature  $T_{bin}$  by block B6 in accordance with Expression (5). Meanwhile, at this stage, the above-described intake-manifold wall temperature  $T_{wallim}$  and intake-manifold heat transfer rate  $\eta_{im}$ , which are variables, are required for obtaining the intake-manifold-outlet gas temperature  $T_{bout}$  by use of Expression (4) (block B4). These variables are obtained as follows.



#### <Obtainment of Intake-Manifold Wall Temperature $T_{wallim}$ >

The intake-manifold wall temperature  $T_{wallim}$  has a strong correlation with the cooling water temperature THW detected by the water temperature sensor 75. Therefore, by means of block B14, the CPU 61 calculates the intake-manifold wall temperature  $T_{wallim}$  in accordance with the following Expression (15), while using a function  $f1T_{wallim}$ , which provides a value that increases with the cooling water temperature THW. Notably, the function  $f1T_{wallim}$  is experimentally obtained in advance and stored in the ROM 62.

$$T_{wallim} = f1T_{wallim}(THW) \quad \dots(15)$$

#### <Obtainment of Intake-Manifold Heat transfer rate $\eta_{im}$ >

As shown in blocks B15 and B16, the CPU 61 calculates the intake-manifold heat transfer rate  $\eta_{im}$  in accordance with the following Expression (16).

$$\left. \begin{array}{l} \eta_{im} = f \eta_{im}(V_{im}, THW) \\ V_{im} = fV_{im}(Gall) \end{array} \right\} \quad \dots(16)$$

In Expression (16),  $V_{im}$  represents the gas flow velocity within the intake manifold (hereinafter referred to as "intake-manifold gas flow velocity  $V_{im}$ "). Since the shape of the intake manifold 31 is known, as shown in the above-described Expression (16), the intake-manifold gas flow velocity  $V_{im}$

can be obtained on the basis of the intake-manifold-inlet gas flow rate  $G_{all}$ . The intake-manifold-inlet gas flow rate  $G_{all}$  is obtained by block B13 in accordance with the above-described Expression (16).

Notably, the intake-manifold gas flow velocity  $V_{im}$  may be obtained directly from an output of a flow velocity sensor disposed in the intake manifold 31. Although the intake-manifold gas flow velocity  $V_{im}$  is used as a variable of the function  $f_{\eta im}$  of Expression (16), in place of the intake-manifold gas flow velocity  $V_{im}$ , the intake-manifold-inlet gas flow rate  $G_{all}$  may be used as a variable.

The above-described Expression (16) is based on the finding that "the intake-manifold heat transfer rate  $\eta_{im}$  is greatly influenced by the gas flow velocity  $V_{im}$  within the intake manifold 31." Although in Expression (16) the cooling water temperature  $THW$  is also used as a variable in order to obtain the intake-manifold heat transfer rate  $\eta_{im}$ , the intake-manifold heat transfer rate  $\eta_{im}$  may be obtained, without use of the cooling water temperature  $THW$ , by use of a function of the intake-manifold gas flow velocity  $V_{im}$  ( $\eta_{im} = f_{\eta im}(V_{im})$ ) or a function of the intake-manifold-inlet gas flow rate  $G_{all}$  ( $\eta_{im} = f_{\eta im}(G_{all})$ ).

Since the function  $f_{\eta im}$  varies among engine models, the function  $f_{\eta im}$  is determined for each model through comparison with actual measurement values. FIG. 11 shows actual measurement values for a certain engine. In the example of FIG. 11, the function  $f_{\eta im}$  is determined as shown in the following Expression (17).

$$\begin{aligned}\eta_{im} &= f \eta_{im}(V_{im}, THW) \\ &= (-0.000061 \cdot THW^2 + 0.003378 \cdot THW - 0.180831) \cdot \ln(V_{im}) \\ &\quad + (0.000048 \cdot THW^2 - 0.000227 \cdot THW + 0.509251) \quad \dots(17)\end{aligned}$$

Through the above-described procedure, the various values ( $T_{bin}$ ,  $\eta_{im}$ ,  $T_{wallim}$ ) required for performing the calculation of Expression (4) are obtained. Thus, the CPU 61 obtains the intake-manifold-outlet gas temperature  $T_{bout}$  by means of block B4 on the basis of Expression (4). Accordingly, the CPU 61 obtains the all-gas flow rate  $G_{cyl}$ , which represents the quantity of all gases taken in the engine 10, by means of block B3 on the basis of Expression (3). Subsequently, the CPU 61 obtains the actual EGR ratio  $R_{act}$  by means of block B1 on the basis of Expression (1).

Next, there will be described various controls of the engines 10, which are performed by use of the various values obtained in the above-described manner.

#### <Fuel Injection Quantity Control and Fuel-Injection Timing Control>

The CPU 61 repeatedly executes, at predetermined intervals, a routine shown by the flowchart of FIG. 12 and adapted to control fuel injection quantity and fuel injection timing. Therefore, when a predetermined timing has been reached, the CPU 61 starts the processing from step 1200, and then proceeds to step 1205 so as to obtain an instruction fuel injection quantity  $q_{fin}$  from the accelerator opening  $Accp$ , the engine speed  $NE$ , and a table (map)  $Mapq_{fin}$  shown in FIG. 13. The table  $Mapq_{fin}$  defines the relation between the accelerator opening  $Accp$  and the engine speed  $NE$ , and the instruction fuel injection quantity  $q_{fin}$ ; and is

stored in the ROM 62.

Subsequently, the CPU 61 proceeds to step 1210 so as to determine a base fuel injection timing  $f_{inj}$  from the instruction fuel injection quantity  $q_{fin}$ , the engine speed  $NE$ , and a table  $Map_{finj}$  shown in FIG. 14. The table  $Map_{finj}$  defines the relation between the instruction fuel injection quantity  $q_{fin}$  and the engine speed  $NE$ , and the base fuel injection timing  $f_{inj}$ ; and is stored in the ROM 62.

Subsequently, the CPU 61 proceeds to step 1215 so as to determine the intake-manifold-outlet gas temperature reference value  $T_{boutref}$  from the instruction fuel injection quantity  $q_{fin}$ , the engine speed  $NE$ , and a table  $Map_{T_{boutref}}$  shown in FIG. 15. The table  $Map_{T_{boutref}}$  defines the relation between the instruction fuel injection quantity  $q_{fin}$  and the engine speed  $NE$ , and the intake-manifold-outlet gas temperature reference value  $T_{boutref}$ ; and is stored in the ROM 62. This intake-manifold-outlet gas temperature reference value  $T_{boutref}$  represents a gas temperature  $T_{bout}$  at the outlet of the intake manifold 31 at the time of employment of the base fuel injection timing  $f_{inj}$  that is determined by use of the table shown in FIG. 14 for the combination of the instruction fuel injection quantity  $q_{fin}$  and the engine speed  $NE$ .

Next, the CPU 61 proceeds to step 1220 so as to determine an injection-timing correction value  $\Delta\theta$  on the basis of the intake-manifold-outlet gas temperature reference value  $T_{boutref}$  determined in step 1215, the difference ( $T_{boutref} - T_{bout}$ ) between the intake-manifold-outlet gas temperature reference value  $T_{boutref}$  and an actual intake-manifold-outlet gas temperature  $T_{bout}$  obtained by block B4 shown in FIG. 3, and a table  $Map_{\Delta\theta}$  shown in FIG. 16. The table  $Map_{\Delta\theta}$  defines the relation between

the difference ( $T_{boutref} - T_{bout}$ ) and the injection-timing correction value  $\Delta\theta$ , and is stored in the ROM 62.

Subsequently, the CPU 61 proceeds to step 1225 so as to correct the base fuel injection timing  $finj$  by the injection-timing correction value  $\Delta\theta$  to thereby obtain a final injection timing  $finj_{final}$ . As described above, the above-described steps 1215 to 1225 correct the injection timing in accordance with the intake-manifold-outlet gas temperature  $T_{bout}$ . In this case, as is apparent from FIG. 16, when the intake-manifold-outlet gas temperature  $T_{bout}$  becomes higher than the intake-manifold-outlet gas temperature reference value  $T_{boutref}$ , the injection-timing correction value  $\Delta\theta$  assumes a negative value corresponding to the difference therebetween, so that the final injection timing  $finj_{final}$  is shifted toward the delay side. In contrast, when the intake-manifold-outlet gas temperature  $T_{bout}$  becomes lower than the intake-manifold-outlet gas temperature reference value  $T_{boutref}$ , the injection-timing correction value  $\Delta\theta$  assumes a positive value corresponding to the difference therebetween, so that the final injection timing  $finj_{final}$  is shifted toward the advance side.

The reason why the injection timing is determined in the above-described manner is as follows. When the intake-manifold-outlet gas temperature  $T_{bout}$  is high, the ignitability of fuel is better than in the case where the temperature  $T_{bout}$  is low. Therefore, even when the fuel injection timing is delayed, the ignitability does not deteriorate, and  $NO_x$  emission can be reduced. In contrast, when the intake-manifold-outlet gas temperature  $T_{bout}$  is low, the ignitability of fuel becomes worse. Therefore, the fuel injection timing is advanced in order to maintain the ignitability. This operation improves the output performance of the engine 10, and

reduces NO<sub>x</sub> emission.

In subsequent step 1230, the CPU 61 determines whether or not the present time coincides with the final injection timing  $finj_{final}$  determined in step 1225. When the present time coincides with the final injection timing  $finj_{final}$ , the CPU 61 proceeds to step 1235 in order to cause the fuel injection valve 21 for a cylinder whose injection timing has been reached to inject fuel in an amount corresponding to the instruction fuel injection quantity  $q_{fin}$  determined in step 1205. Subsequently, the CPU 61 proceeds to step 1295 so as to end the present routine. When the result of the determination in step 1230 is "No," the CPU 61 proceeds directly to step 1295 so as to end the present routine. Through the above-described processing, fuel injection quantity control and fuel injection timing control are achieved.

#### <EGR control>

Next, EGR ratio control will be described. The CPU 61 repeatedly executes, at predetermined intervals, a routine shown by the flowchart of FIG. 17 and adapted to control the EGR ratio. Therefore, when a predetermined timing has been reached, the CPU 61 starts the processing from step 1700, and then proceeds to step 1705 so as to determine a target intake oxygen concentration  $O2_{tgt}$  from the instruction fuel injection quantity  $q_{fin}$  at the present time, the engine speed  $NE$  at the present time, and a table  $MapO2_{tgt}$  shown in the block of the present step. The table  $MapO2_{tgt}$  defines the relation between the instruction fuel injection quantity  $q_{fin}$  and the engine speed  $NE$ , and the target intake oxygen concentration  $O2_{tgt}$ ; and is stored in the ROM 62.

Subsequently, in step 1710, the CPU 61 obtains a supply fuel quantity  $Q$  per unit time from the instruction fuel injection quantity  $q_{fin}$  and the engine speed  $NE$ ; and in subsequent step 1715, the CPU 61 obtains an air surplus ratio  $\lambda$  by the expression ( $\lambda = k\lambda \cdot Ga_{act}/Q$ ) shown in the block of the present step.  $k\lambda$  is a constant. In subsequent step 1720, the CPU 61 obtains a target EGR ratio  $R_{tgt}$  on the basis of the target intake oxygen concentration  $O2_{tgt}$  determined in the above-described step 1705, the air surplus ratio  $\lambda$  obtained in the above-described step 1720, and the expression ( $R_{tgt} = \lambda \cdot (p \cdot O2_{tgt} + q)$ , where  $p$  and  $q$  are constants) shown in the block of step 1720. Notably, the relation among intake oxygen concentration, EGR ratio, and air surplus ratio is disclosed in detail in, for example, Japanese Patent Application Laid-Open (*koka*) No. 10-141147.

Next, in step 1725, the CPU 61 determines whether or not the actual EGR ratio  $R_{act}$  obtained in block B1 shown in FIG. 3 is greater than the target EGR ratio  $R_{tgt}$  obtained in the above-described step 1720. When the result of the determination in step 1725 is "Yes," the CPU 61 proceeds to step 1730 in order to close the EGR control valve 52 by a predetermined amount, to thereby reduce the EGR ratio. Subsequently, the CPU 61 proceeds to step 1795 so as to end the present routine. In contrast, when the result of the determination in step 1725 is "No," the CPU 61 proceeds to step 1735 in order to open the EGR control valve 52 by a predetermined amount, to thereby increase the EGR ratio. Subsequently, the CPU 61 proceeds to step 1795. By virtue of the above operation, the EGR ratio is controlled in such a manner that the actual intake oxygen concentration becomes equal to the target intake oxygen concentration  $O2_{tgt}$ , whereby emission of  $NO_x$  and smoke can be reduced.

In the EGR ratio control by the routine shown in FIG. 17, the CPU 61 controls the EGR ratio by obtaining the target intake oxygen concentration  $O2tgt$ , and converting the target intake oxygen concentration  $O2tgt$  to the target EGR ratio  $Rtgt$ . However, the EGR ratio may be controlled as follows. The target EGR ratio  $Rtgt$  is obtained directly from an actual instruction fuel injection quantity  $qfin$ , an actual engine speed  $NE$ , and a table  $MapRtgt$  shown in FIG. 18 and defining the relation between the instruction fuel injection quantity  $qfin$  and the engine speed  $NE$ , and the target EGR ratio  $Rtgt$ ; and the opening of the EGR control valve 52 is controlled in such a manner that the actual EGR ratio  $Ract$  becomes equal to the target EGR ratio  $Rtgt$ .

#### <Boost Pressure Control>

Next, boost pressure control will be described. The CPU 61 repeatedly executes, at predetermined intervals, an unillustrated routine for controlling boost pressure so as to determine, at predetermined intervals, a target boost pressure  $Pbtgt$ , from the instruction fuel injection quantity  $qfin$  at the present time, the engine speed  $NE$  at the present time, and a table  $MapPbtgt$  shown in FIG. 19. The table  $MapPbtgt$  defines the relation between the instruction fuel injection quantity  $qfin$  and the engine speed  $NE$ , and the target boost pressure  $Pbtgt$ ; and is stored in the ROM 62.

Subsequently, the CPU 61 compares the determined target boost pressure  $Pbtgt$  and the actual boost pressure  $Pb$  obtained from the intake pressure sensor 73, and controls the opening of the turbocharger throttle valve 35c in such a manner that the actual boost pressure  $Pb$  becomes equal to the target boost pressure  $Pbtgt$ . The boost pressure control is



executed in this manner.

As described above, in the embodiment of the engine control apparatus according to the present invention, since the cooling efficiency of the EGR-gas cooling apparatus 53 is obtained on the basis of the exhaust-circulation-pipe-inlet EGR-gas temperature and the EGR-gas-flow-rate corresponding value, the estimation accuracy of the exhaust-circulation-pipe-outlet EGR-gas temperature is improved. Further, since the intake-manifold-outlet gas temperature  $T_{bout}$  is estimated in consideration of heat exchange between the intake manifold 31 and a mixture gas (intake air) of new air and EGR gas, the estimation accuracy of the intake-manifold-outlet gas temperature  $T_{bout}$  is also improved. As a result, the EGR ratio can be estimated accurately.

Moreover, in the above-described embodiment, an error which is contained in the provisional EGR gas flow rate  $G_{egr0}$  obtained by use of a general formula regarding the flow rate of a compressible fluid passing through a throttle portion and which is caused by the pipe friction is corrected by use of the correction value  $dP_{gain}$ . As a result, the present apparatus can accurately estimate the flow rate  $G_{egr}$  of EGR gas flowing into the intake passage (passing through the EGR control valve 52), even when the difference between the obtained gas pressure ( $P_{ex}$ ) on the upstream side of the throttle portion and the obtained gas pressure ( $P_b$ ) on the downstream side of the throttle portion decreases, resulting in a strong tendency that, rather than the degree of throttle, the pipe friction predominantly determines the EGR gas flow rate.

The present invention is not limited to the above-described embodiment, and may be modified in various manners within the scope of

the present invention. For example, the exhaust-manifold gas pressure  $P_{ex}$  may be obtained on the basis of an output value of an exhaust pressure sensor (exhaust-circulation-pipe-inlet EGR gas pressure obtaining means) disposed in the vicinity of a location at which the exhaust manifold 41 is connected to the exhaust circulation pipe 51.

The above-described correction coefficient  $dP_{gain}$  may be obtained on the basis of both the effective opening area  $A_{egr}$  and the differential pressure  $dP$ . That is, the provisional EGR flow rate  $G_{egr0}$  may be corrected in accordance with the effective opening area  $A_{egr}$  and the differential pressure  $dP$ .